Lecture 3: Three-phase power circuits

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Introduction

Almost all electric power generation and most of the power transmission in the world is in the form of three-phase AC circuits. A three-phase AC system consists of three-phase generators, transmission lines, and loads.

There are two major advantages of three-phase systems over a single-phase system:  
1) More power per kilogram of metal form a three-phase machine;  
2) Power delivered to a three-phase load is constant at all time, instead of pulsing as it does in a single-phase system.

The first three-phase electrical system was patented in 1882 by John Hopkinson - British physicist, electrical engineer, Fellow of the Royal Society.
1. Generation of three-phase voltages and currents

A three-phase generator consists of three single-phase generators with voltages of equal amplitudes and phase differences of $120^0$.

Each of three-phase generators can be connected to one of three identical loads. This way the system would consist of three single-phase circuits differing in phase angle by $120^0$.

The current flowing to each load can be found as

$$I = \frac{V}{Z} \quad (3.4.1)$$
1. Generation of three-phase voltages and currents

Therefore, the currents flowing in each phase are

\[ I_A = \frac{V_{\angle 0^\circ}}{Z_{\angle \theta}} = I_{\angle -\theta} \]  \hspace{1cm} (3.5.1)

\[ I_B = \frac{V_{\angle -120^\circ}}{Z_{\angle \theta}} = I_{\angle -120 - \theta} \]  \hspace{1cm} (3.5.2)

\[ I_C = \frac{V_{\angle -240^\circ}}{Z_{\angle \theta}} = I_{\angle -240 - \theta} \]  \hspace{1cm} (3.5.3)

1. Generation of three-phase voltages and currents

We can connect the negative (ground) ends of the three single-phase generators and loads together, so they share the common return line (neutral).
1. Generation of three-phase voltages and currents

The current flowing through a neutral can be found as

\[ I_N = I_A + I_B + I_C = I \angle -\theta + I \angle -\theta -120^\circ + I \angle -\theta -240^\circ \]

\[ = I \cos(-\theta) + jI \sin(-\theta) + I \cos(-\theta -120^\circ) + jI \sin(-\theta -120^\circ) + I \cos(-\theta -240^\circ) + jI \sin(-\theta -240^\circ) \]

\[ = I \left[ \cos(-\theta) + \cos(-\theta -120^\circ) + \cos(-\theta -240^\circ) \right] + jI \left[ \sin(-\theta) + \sin(-\theta -120^\circ) + \sin(-\theta -240^\circ) \right] \]

\[ = I \left[ \cos(-\theta) + \cos(-\theta) \cos(120^\circ) + \sin(-\theta) \sin(120^\circ) + \cos(-\theta) \cos(240^\circ) + \sin(-\theta) \sin(240^\circ) \right] \]

\[ + jI \left[ \sin(-\theta) + \sin(-\theta) \cos(120^\circ) - \cos(-\theta) \sin(120^\circ) + \sin(-\theta) \cos(240^\circ) - \cos(-\theta) \sin(240^\circ) \right] \]

Which is:

\[ I_N = I \left[ \cos(-\theta) - \frac{1}{2} \cos(-\theta) + \frac{\sqrt{3}}{2} \sin(-\theta) - \frac{1}{2} \cos(-\theta) - \frac{\sqrt{3}}{2} \sin(-\theta) \right] \]

\[ + jI \left[ \sin(-\theta) - \frac{1}{2} \sin(-\theta) + \frac{\sqrt{3}}{2} \cos(-\theta) - \frac{1}{2} \sin(-\theta) - \frac{\sqrt{3}}{2} \cos(-\theta) \right] \]

\[ = 0 \]

As long as the three loads are equal, the return current in the neutral is zero!

Such three-phase power systems (equal magnitude, phase differences of 120°, identical loads) are called balanced.

In a balanced system, the neutral is unnecessary!

Phase Sequence is the order in which the voltages in the individual phases peak.
Voltages and currents

There are two types of connections in three-phase circuits: Y and Δ.

Each generator and each load can be either Y- or Δ-connected. Any number of Y- and Δ-connected elements may be mixed in a power system.

Phase quantities - voltages and currents in a given phase.
Line quantities – voltages between the lines and currents in the lines connected to the generators.

1. Y-connection

Assuming a resistive load…
Voltages and currents

1. Y-connection (cont)

\[ V_{an} = V_φ \angle 0^0 \]
\[ V_{bn} = V_φ \angle -120^0 \]
\[ V_{cn} = V_φ \angle -240^0 \] (3.11.1)

Since we assume a resistive load:

\[ I_a = I_φ \angle 0^0 \]
\[ I_b = I_φ \angle -120^0 \]
\[ I_c = I_φ \angle -240^0 \] (3.11.2)

Voltages and currents

1. Y-connection (cont 2)

The current in any line is the same as the current in the corresponding phase.

\[ I_L = I_φ \] (3.12.1)

Voltages are:

\[ V_{ab} = V_a - V_φ = V_φ \angle 0^0 - V_φ \angle -120^0 = V_φ - \left( -\frac{1}{2}V_φ - j\frac{\sqrt{3}}{2}V_φ \right) = \frac{3}{2}V_φ + j\frac{\sqrt{3}}{2}V_φ \]

\[ = \sqrt{3}V_φ \left( \frac{\sqrt{3}}{2} + j\frac{1}{2} \right) = \sqrt{3}V_φ \angle 30^0 \] (3.12.2)
Voltages and currents

1. Y-connection (cont 3)

Magnitudes of the line-to-line voltages and the line-to-neutral voltages are related as:

\[ V_{LL} = \sqrt{3} V_\phi \] (3.13.1)

In addition, the line voltages are shifted by 30° with respect to the phase voltages.

In a connection with abc sequence, the voltage of a line leads the phase voltage.

Voltages and currents

1. Δ-connection

assuming a resistive load:

\[ V_{ab} = V_\phi < 0^\circ \]
\[ V_{bc} = V_\phi < -120^\circ \] (3.14.1)
\[ V_{ca} = V_\phi < -240^\circ \]
\[ I_{ab} = I_\phi < 0^\circ \]
\[ I_{bc} = I_\phi < -120^\circ \] (3.14.2)
\[ I_{ca} = I_\phi < -240^\circ \]
Voltages and currents

1. Δ-connection (cont)

\[ V_{LL} = V_\phi \]  

(3.15.1)

The currents are:

\[ I_a = I_{\alpha} - I_{\alpha} = I_\phi \angle 0^0 - I_\phi \angle 240^0 = I_\phi - \left( -\frac{1}{2} I_\phi + j\frac{\sqrt{3}}{2} I_\phi \right) \]
\[ = \frac{3}{2} I_\phi - j\frac{\sqrt{3}}{2} I_\phi = \sqrt{3} I_\phi \left( \frac{\sqrt{3}}{2} - j\frac{1}{2} \right) = \sqrt{3} I_\phi \angle -30^0 \]  

(3.15.2)

The magnitudes:

\[ I_L = \sqrt{3} I_\phi \]  

(3.15.3)

Voltages and currents

For the connections with the abc phase sequences, the current of a line lags the corresponding line current by 30°.
**Power relationships**

For a balanced Y-connected load with the impedance $Z = Z_\phi \angle \theta$:

and voltages:

\[ v_a(t) = \sqrt{2}V \sin \omega t \]
\[ v_b(t) = \sqrt{2}V \sin(\omega t - 120^\circ) \]
\[ v_c(t) = \sqrt{2}V \sin(\omega t - 240^\circ) \]  \hspace{1cm} (3.17.1)

The currents can be found:

\[ i_a(t) = \sqrt{2}I \sin(\omega t - \theta) \]
\[ i_b(t) = \sqrt{2}I \sin(\omega t - 120^\circ - \theta) \]
\[ i_c(t) = \sqrt{2}I \sin(\omega t - 240^\circ - \theta) \]  \hspace{1cm} (3.17.2)

The instantaneous power is:

\[ p(t) = v(t)i(t) \]  \hspace{1cm} (3.18.1)

Therefore, the instantaneous power supplied to each phase is:

\[ p_a(t) = v_a(t)i_a(t) = 2VI \sin(\omega t) \sin(\omega t - \theta) \]
\[ p_b(t) = v_b(t)i_b(t) = 2VI \sin(\omega t - 120^\circ) \sin(\omega t - 120^\circ - \theta) \]  \hspace{1cm} (3.18.2)
\[ p_c(t) = v_c(t)i_c(t) = 2VI \sin(\omega t - 240^\circ) \sin(\omega t - 240^\circ - \theta) \]

Since

\[ \sin\alpha \sin\beta = \frac{1}{2} [\cos(\alpha - \beta) - \cos(\alpha + \beta)] \]  \hspace{1cm} (3.18.3)
Power relationships

Therefore

\[
p_a(t) = VI \left[ \cos \theta - \cos(2 \omega t - \theta) \right]
\]
\[
p_b(t) = VI \left[ \cos \theta - \cos(2 \omega t - 240^\circ - \theta) \right]
\]
\[
p_c(t) = VI \left[ \cos \theta - \cos(2 \omega t - 480^\circ - \theta) \right]
\]  

(3.19.1)

The total power on the load

\[
p_{tot}(t) = p_a(t) + p_b(t) + p_c(t) = 3VI \cos \theta
\]

(3.19.2)

The pulsing components cancel each other because of 120° phase shifts.

Power relationships

The instantaneous power in phases.

The total power supplied to the load is constant.
Power relationships

Phase quantities in each phase of a Y- or Δ-connection.

Real

\[ P = 3V_{\phi}I_{\phi} \cos \theta = 3I_{\phi}^2Z \cos \theta \]  

(3.21.1)

Reactive

\[ Q = 3V_{\phi}I_{\phi} \sin \theta = 3I_{\phi}^2Z \sin \theta \]  

(3.21.1)

Apparent

\[ S = 3V_{\phi}I_{\phi} = 3I_{\phi}^2Z \]  

(3.21.1)

Note: these equations are only valid for a balanced load.

Power relationships

Line quantities: Y-connection.

Power consumed by a load:

\[ P = 3V_{\phi}I_{\phi} \cos \theta \]  

(3.22.1)

Since for this load

\[ I_L = I_{\phi} \quad \text{and} \quad V_L = \sqrt{3}V_{\phi} \]  

(3.22.2)

Therefore:

\[ P = \frac{3V_{LL}}{\sqrt{3}} I_L \cos \theta \]  

(3.22.3)

Finally:

\[ P = \sqrt{3}V_{LL}I_L \cos \theta \]  

(3.22.4)

Note: these equations were derived for a balanced load.
Power relationships

Line quantities: Δ-connection.

Power consumed by a load: \[ P = 3V_f I_f \cos \theta \]  
(3.23.1)

Since for this load \[ I_L = \sqrt{3}I_f \text{ and } V_{LL} = V_f \]  
(3.23.2)

Therefore: \[ P = \frac{3I_L}{\sqrt{3}}V_{LL} \cos \theta \]  
(3.23.3)

Finally: \[ P = \sqrt{3}V_{LL} I_L \cos \theta \]  
(3.23.4)

Same as for a Y-connected load!

Note: these equations were derived for a balanced load.

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Power relationships

Line quantities: Y- and Δ-connection.

Reactive power \[ Q = \sqrt{3}V_{LL} I_L \sin \theta \]  
(3.24.1)

Apparent power \[ S = \sqrt{3}V_{LL} I_L \]  
(3.24.2)

Note: \( \theta \) is the angle between the phase voltage and the phase current.
Analysis of balanced systems

We can determine voltages, currents, and powers at various points in a balanced circuit.

Consider a Y-connected generator and load via three-phase transmission line.

For a balanced Y-connected system, insertion of a neutral does not change the system. All three phases are identical except of 120° shift. Therefore, we can analyze a single phase (per-phase circuit).

Limitation: not valid for Δ-connections...

A Δ-connected circuit can be analyzed via the transform of impedances by the Y-Δ transform. For a balanced load, it states that a Δ-connected load consisting of three equal impedances Z is equivalent to a Y-connected load with the impedances Z/3. This equivalence implies that the voltages, currents, and powers supplied to both loads would be the same.
Analysis of balanced systems: Ex

Example 3-1:

for a 208-V three-phase ideal balanced system, find:

a) the magnitude of the line current $I_L$;

b) The magnitude of the load's line and phase voltages $V_{LL}$ and $V_{φL}$;

c) The real, reactive, and the apparent powers consumed by the load;

d) The power factor of the load.

Analysis of balanced systems

Both, the generator and the load are Y-connected, therefore, it's easy to construct a per-phase equivalent circuit...

a) The line current:

$$I_L = \frac{V}{Z_L + Z_{load}} = \frac{120\angle 0^\circ}{(0.06 + j0.12) + (12 + j9)} = \frac{120\angle 0^\circ}{15.12\angle 37.1^\circ} = 7.94\angle -37.1^\circ \ A$$

b) The phase voltage on the load:

$$V_{φL} = I_LZ_{φL} = (7.94\angle -37.1^\circ)(12 + j9) = (7.94\angle -37.1^\circ)(15\angle 36.9^\circ) = 119.1\angle -0.2^\circ \ V$$

The magnitude of the line voltage on the load:

$$V_{LL} = \sqrt{3}V_{φL} = 206.3 \ V$$
Analysis of balanced systems

c) The real power consumed by the load:

\[ P_{load} = 3V_{\phi}I_{\phi} \cos \theta = 3 \cdot 119.1 \cdot 7.94 \cos 36.9^0 = 2270 \text{ W} \]

The reactive power consumed by the load:

\[ Q_{load} = 3V_{\phi}I_{\phi} \sin \theta = 3 \cdot 119.1 \cdot 7.94 \sin 36.9^0 = 1702 \text{ var} \]

The apparent power consumed by the load:

\[ S_{load} = 3V_{\phi}I_{\phi} = 3 \cdot 119.1 \cdot 7.94 = 2839 \text{ VA} \]

d) The load power factor:

\[ PF_{load} = \cos \theta = \cos 36.9^0 = 0.8 \text{ – lagging} \]

One-line diagrams

Since, in a balanced system, three phases are similar except of the 120° phase shift, power systems are frequently represented by a single line representing all three phases of the real system.

This is a one-line diagram.

Such diagrams usually include all the major components of a power system: generators, transformers, transmission lines, loads.
Using the power triangle

If we can neglect the impedance of the transmission line, an important simplification in the power calculation is possible.

If the generator voltage in the system is known, then we can find the current and power factor at any point in the system as follows:

1. The line voltages at the generator and the loads will be identical since the line is lossless.
2. Real and reactive powers on each load.
3. The total real and reactive powers supplied to all loads from the point examined.
4. The system power factor at that point using the power triangle relationship.
5. Line and phase currents at that point.

We can treat the line voltage as constant and use the power triangle method to quickly calculate the effect of adding a load on the overall system and power factor.